

# The importance of friction in mountain wave drag enhancement by parametric resonance

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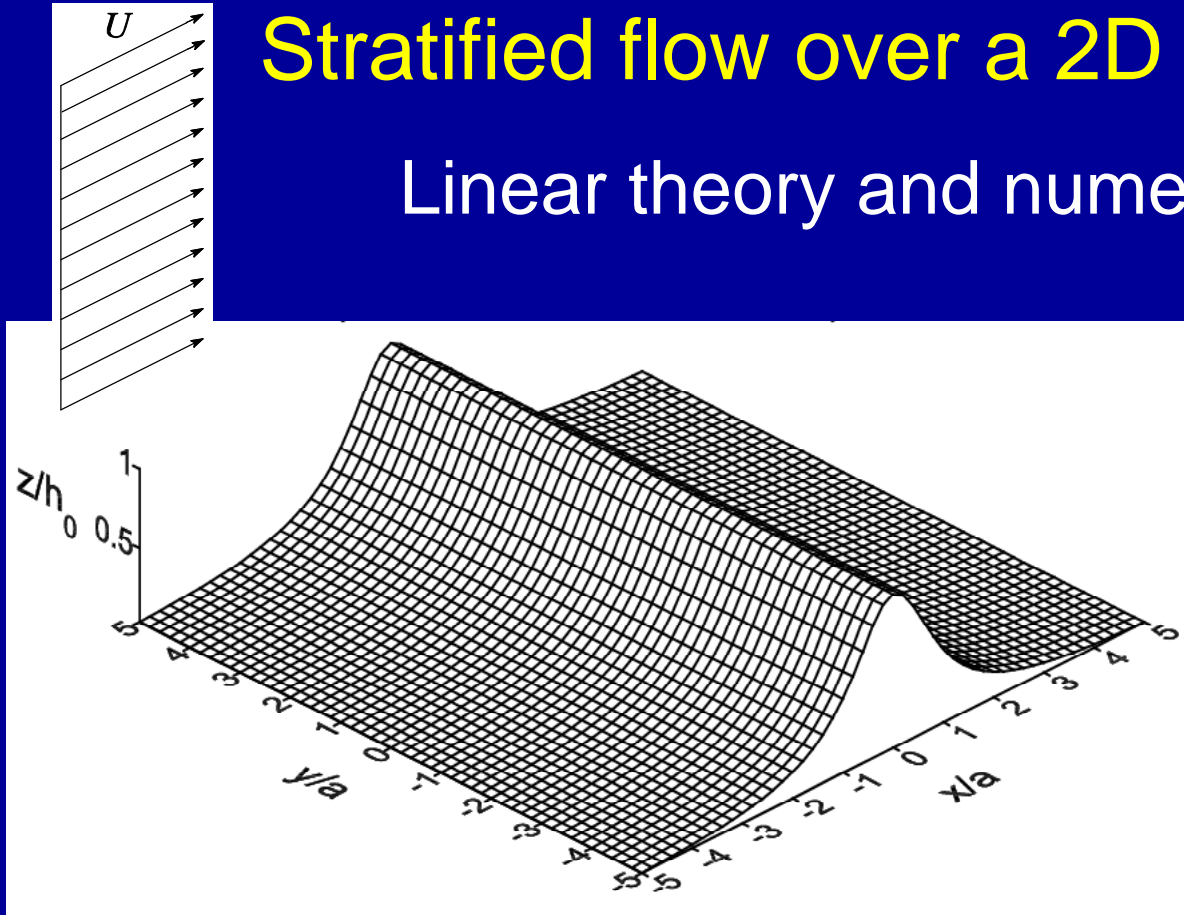


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# Stratified flow over a 2D mountain

Linear theory and numerical simulations



Bell-shaped ridge

$$h = \frac{h_0}{1 + (x/a)^2}$$

Basic Scorer

parameter:  $l_0 = N/U$

$$N^2 = \frac{g}{\theta_0} \frac{d\bar{\theta}}{dz}$$

## Linear model

- Boussinesq approximation
- Linearization ( $l_0 h_0 \ll 1$ )
- Non-hydrostatic flow ( $l_0 a \neq \infty$ )
- Viscous processes represented by Rayleigh damping  $\lambda^{-2}$

# Linear model

$$\hat{w}'' + \left( \frac{l^2}{1 - i\lambda/Uk} - k^2 \right) \hat{w} = 0$$

Taylor-Goldstein equation

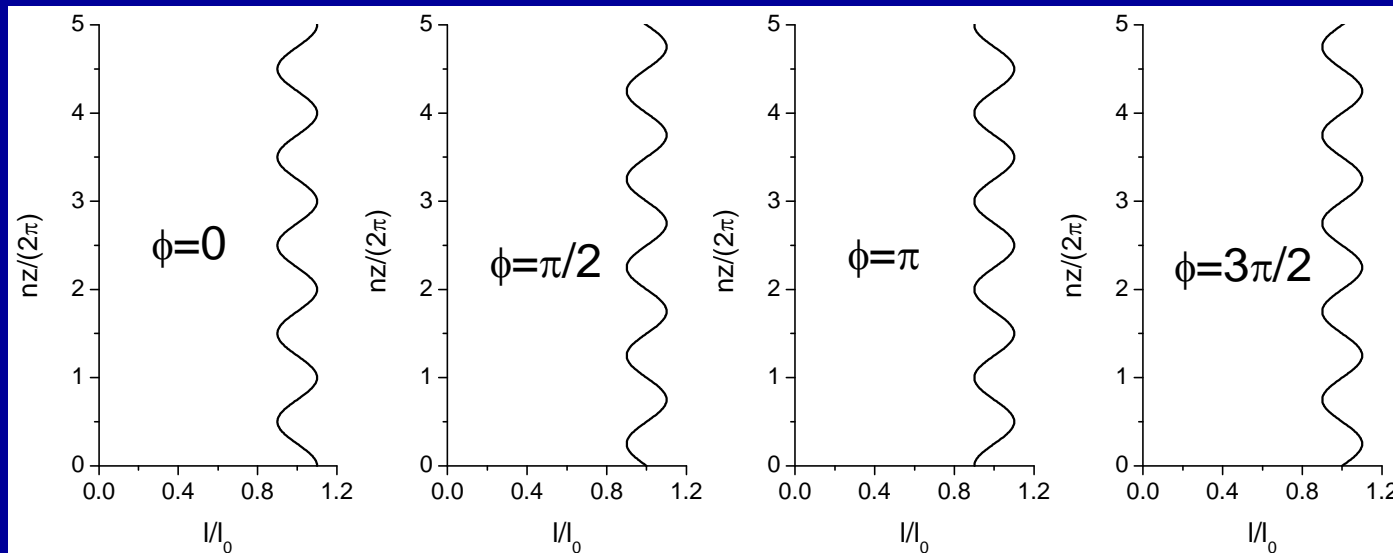
- Boundary condition at surface:
- Radiation or decay boundary condition aloft

$$\hat{w}(z=0) = iUk\hat{h}$$

Used Scorer parameter profiles:

$$l^2 = l_0^2 [1 + \varepsilon \cos(nz + \phi)]$$

$$\varepsilon = 0.1$$



Calculation of gravity wave drag:

$$D = \int_{-\infty}^{+\infty} p(z=0) \frac{\partial h}{\partial x} dx = 2\pi i \int_{-\infty}^{+\infty} k \hat{p}^*(z=0) \hat{h} dk$$

# Solution procedure

Expand solution in power series of  $\varepsilon$ :

$$\hat{W} = \hat{W}_0 + \varepsilon \hat{W}_1 + \varepsilon^2 \hat{W}_2 + \dots$$

Drag is also power series of  $\varepsilon$ :

$$D = D_0 + \varepsilon D_1 + \varepsilon^2 D_2 + \dots$$

It is sufficient to expand  $D$  up to first order:

$$\frac{D}{D_0} = 1 + \varepsilon \frac{D_1}{D_0} = 1 + 2\varepsilon \frac{\int_0^{+\infty} k' e^{-2k'} m'_R \frac{(4m'^2_R + 4m'^2_I - n'^2) \cos \phi - 4n' m'_I \sin \phi}{(4m'^2_R - 4m'^2_I - n'^2)^2 + 64m'^2_R m'^2_I} dk'}{\int_0^{+\infty} k' e^{-2k'} (m'_R + \lambda a / (Uk')) m'_I dk'}$$

$$k' = ka$$

$$n' = n / l_0$$

$$m'_R = m_R / l_0$$

$$m'_I = m_I / l_0$$

$$m = m_R + im_I$$

Vertical wavenumber of internal gravity waves

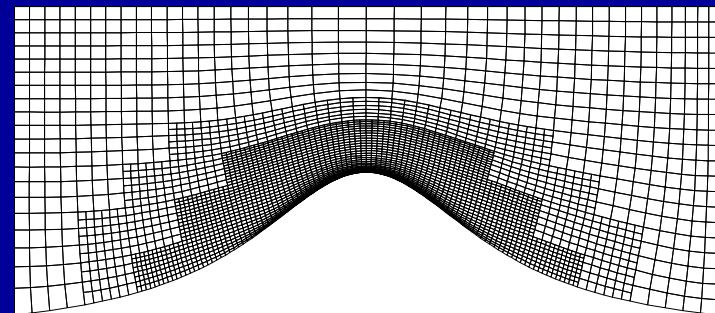
Normalized drag  $D/D_0$  is function of:  $\varepsilon, n/l_0, \phi, l_0 a, \lambda a/U$

# Numerical simulations

Use 2D nonlinear nonhydrostatic model called FLEX  
(Argaín et al. 2009, *BLM*)

- Finite difference method, with implicit time integration
- Terrain-following grid with 192 x 525 grid points
- Domain of **240 km** in horizontal and **44 km** in vertical
- Local grid refinement near surface with  $\Delta z \sim \mathbf{32\ m}$
- Sponges with Rayleigh damping at lateral and top boundaries
- Raymond & Kuo boundary condition at lateral boundaries
- 4th-order spatial filter applied every 3 time steps
- $\Delta t = \mathbf{2\ s}$ , integration time up to 69 h, typically 17 h.

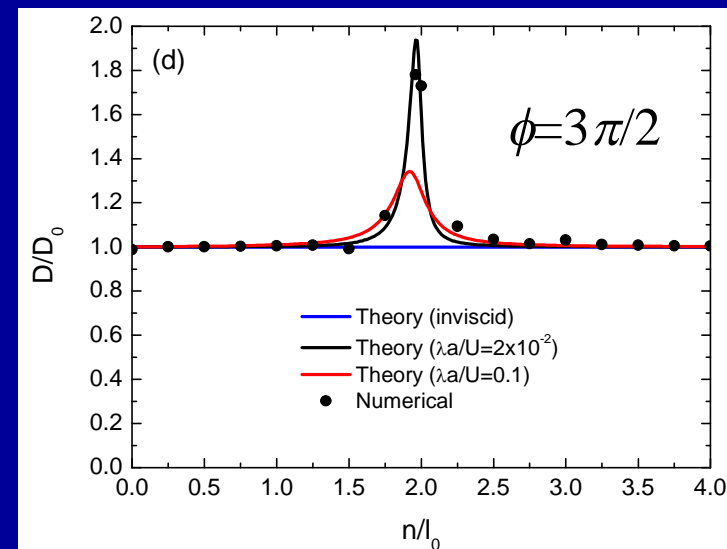
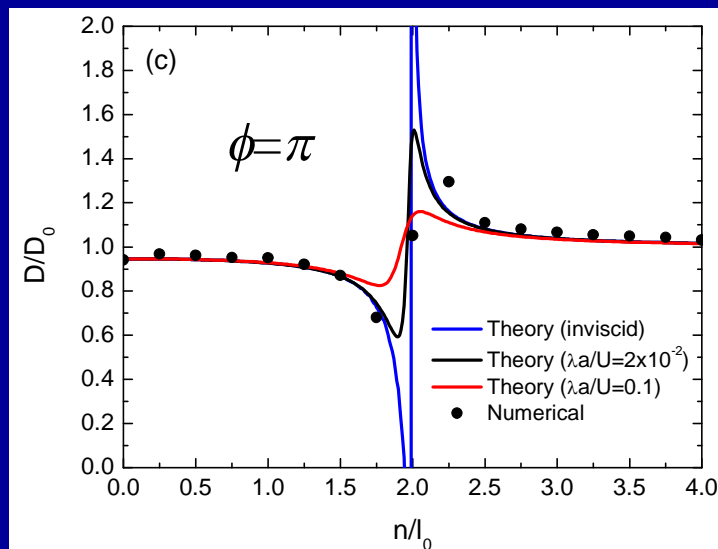
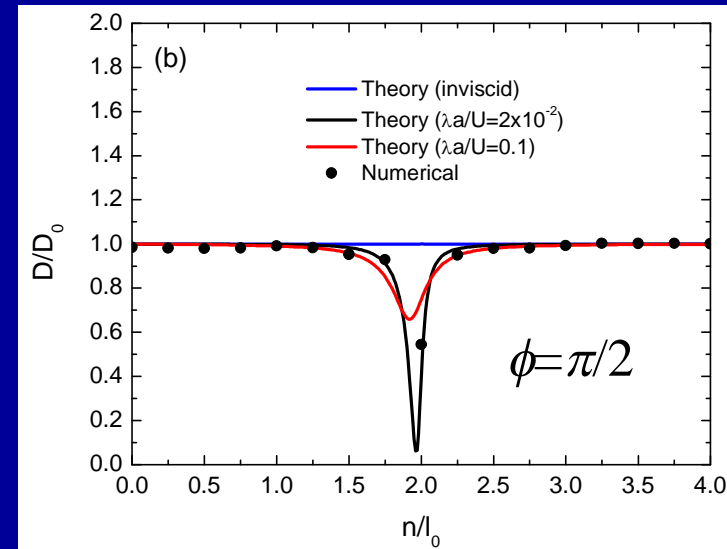
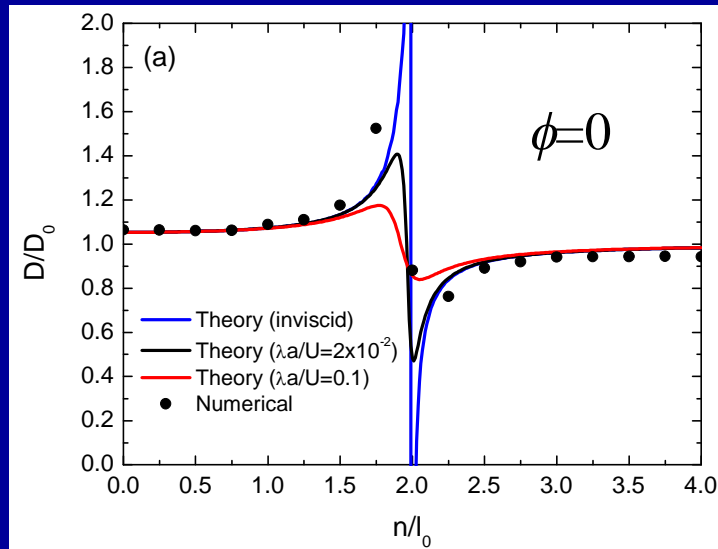
- Anelastic approximation used
- Inviscid flow (no turbulence closure)
- Free-slip surface boundary condition
- $\mathbf{U=20\ m/s}$ ,  $\mathbf{N=0.01\ s^{-1}}$ ,  $\mathbf{a=4,10,20\ km}$ ,  $\mathbf{h_0=10\ m}$
- $\mathbf{l_0 a=2,5,10}$ ,  $\mathbf{l_0 h_0=5 \times 10^{-3}}$  (strongly linear flow)



# Results - Effect of friction

$$l_0 a = 5$$

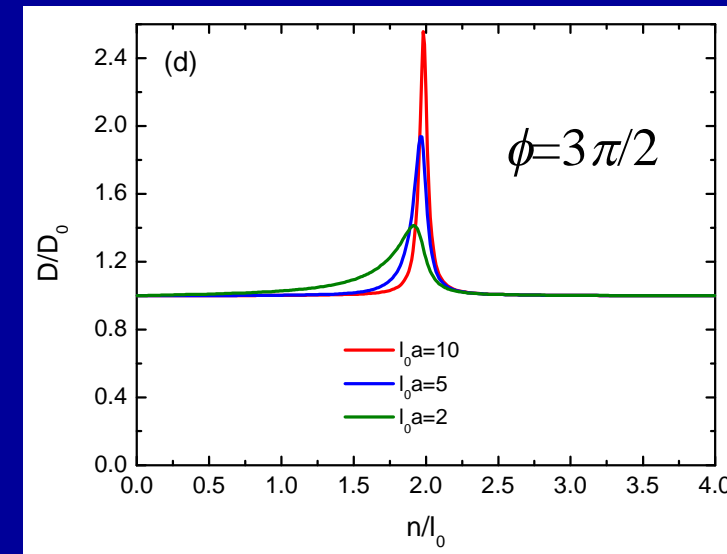
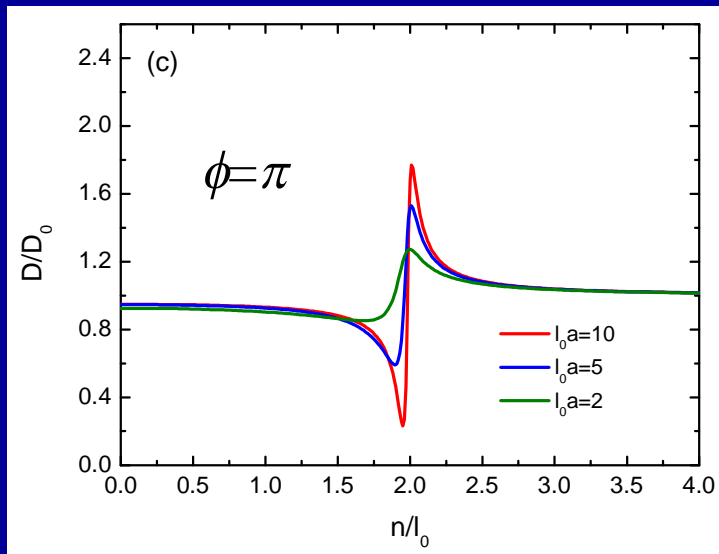
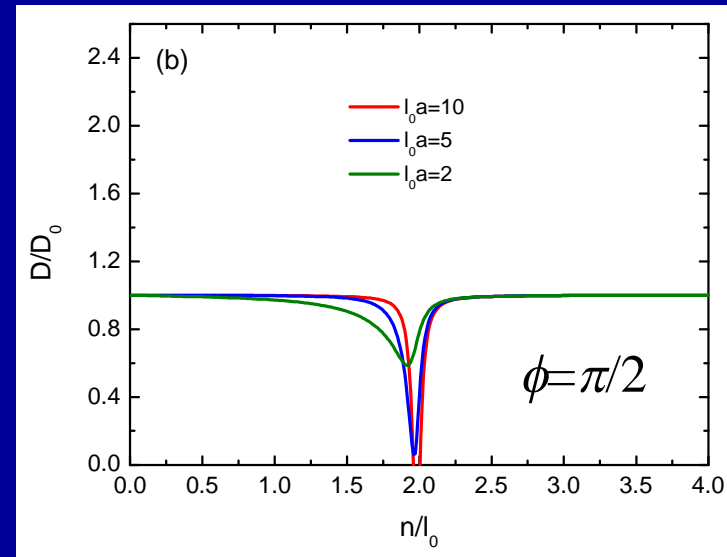
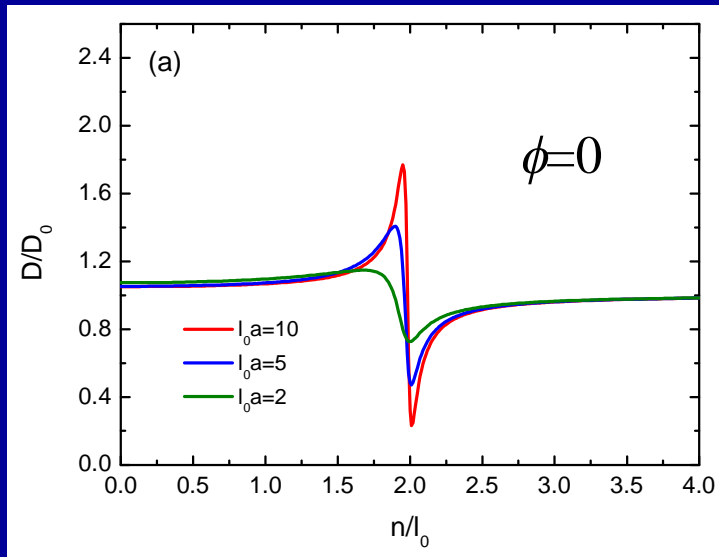
$$\varepsilon = 0.1$$



# Non-hydrostatic effects (analytical)

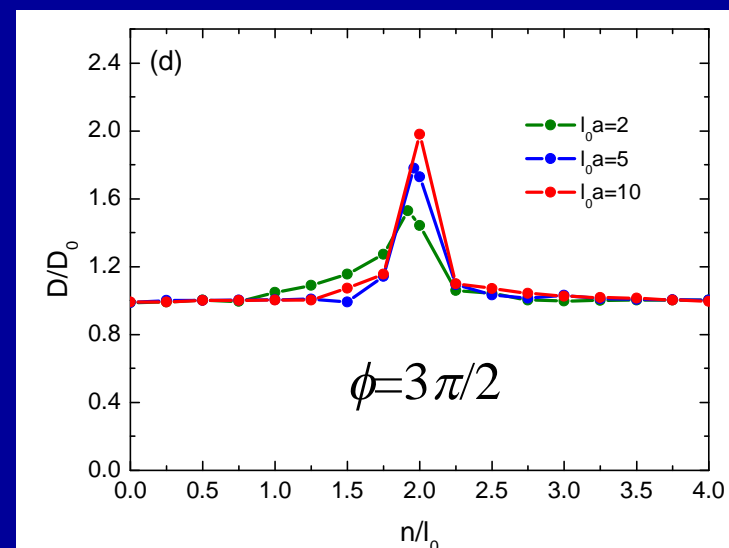
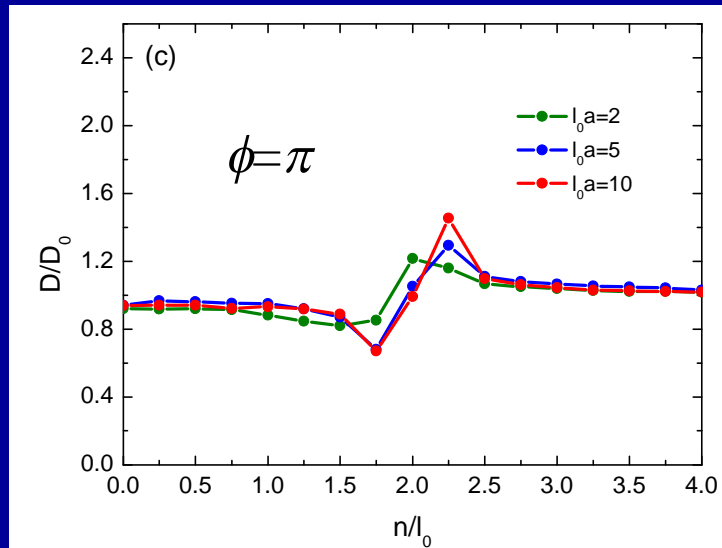
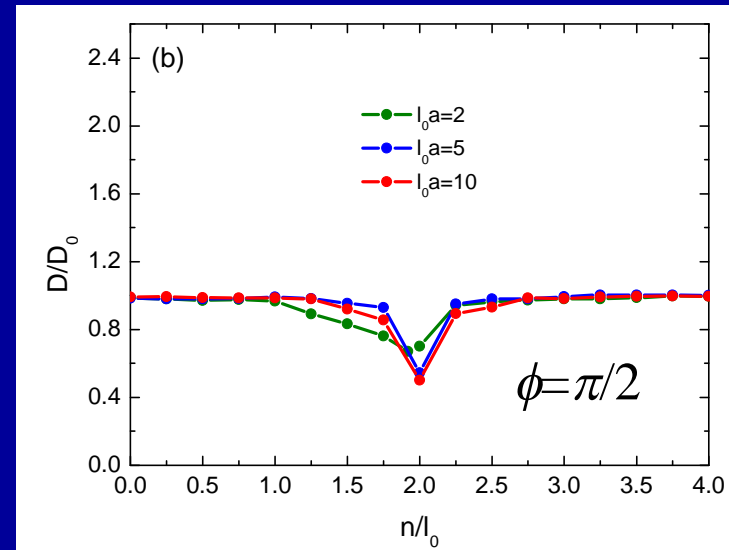
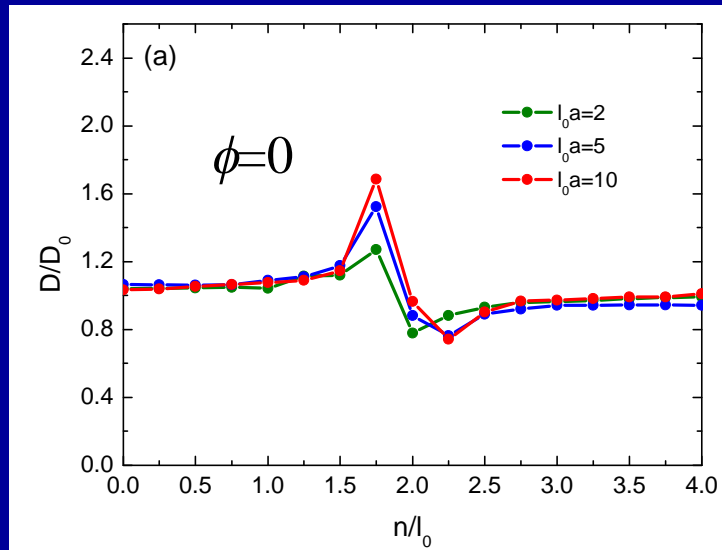
$\varepsilon = 0.1$

$\lambda a / U = 2 \times 10^{-2}$



# Non-hydrostatic effects (numerical)

$\varepsilon = 0.1$





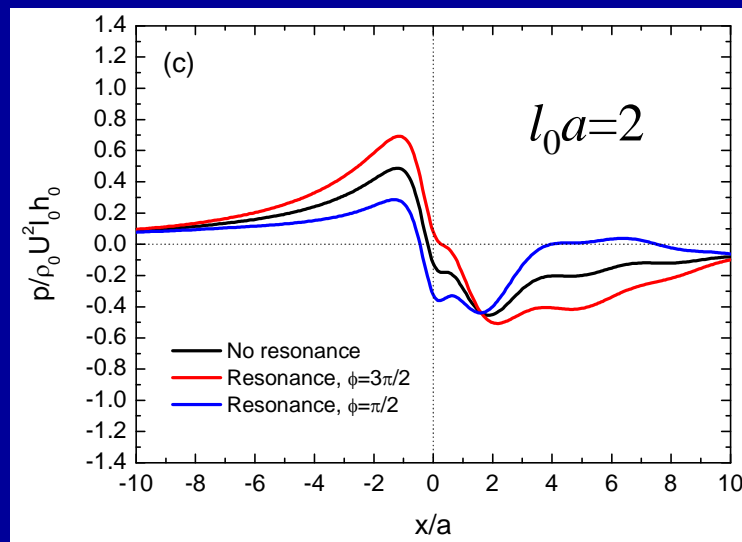
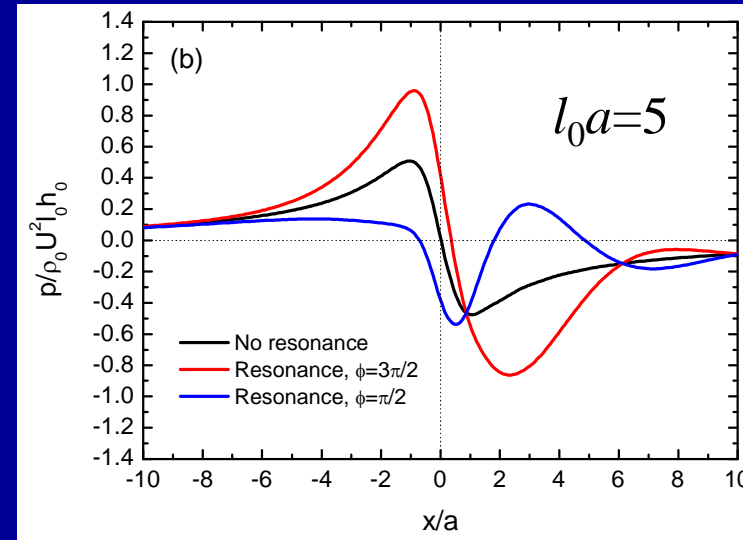
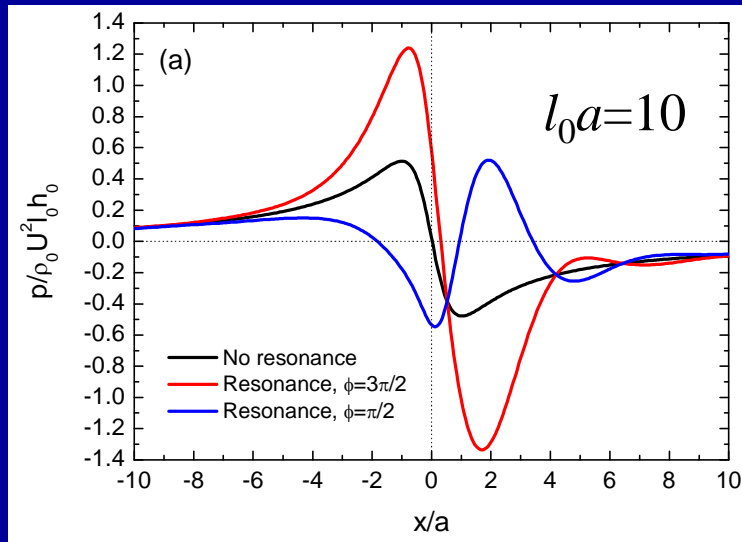
# Pressure perturbation (analytical)

$\varepsilon = 0.1$

$n/l_0 = 2$

Normalized pressure perturbation,  $p/[\rho_0 U^2 l_0 h_0]$

$\lambda a / U = 2 \times 10^{-2}$



- Pressure perturbation more symmetric (low drag) when  $\phi = \pi/2$ , and more antisymmetric (high drag) when  $\phi = 3\pi/2$
- Effect becomes weaker as  $l_0 a$  decreases

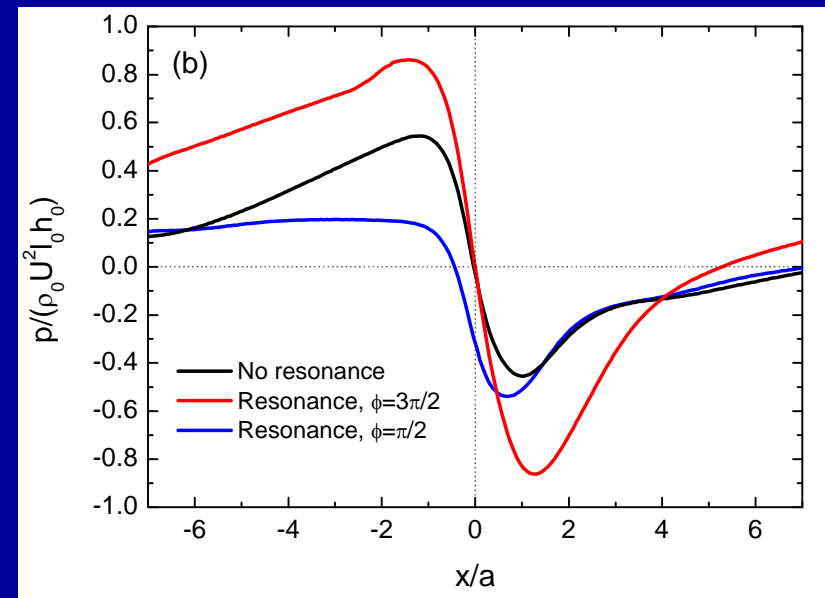
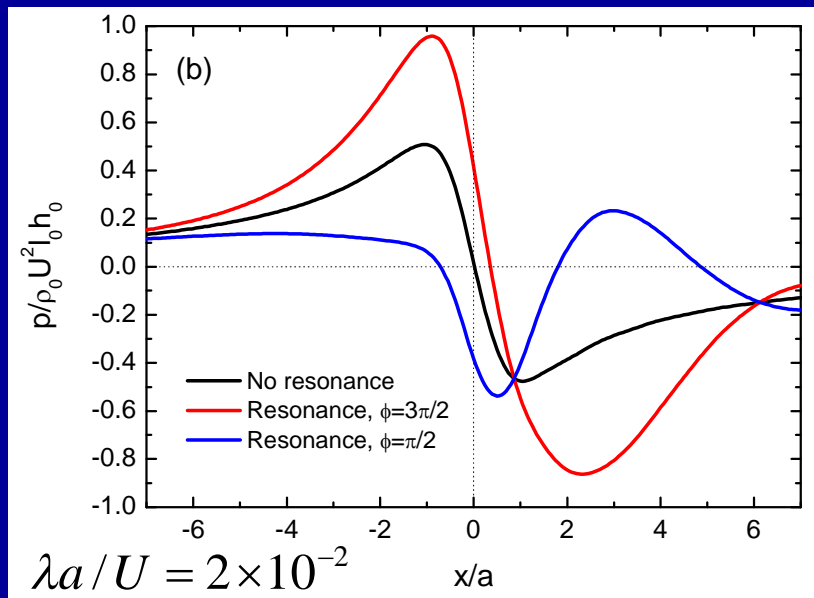
# Pressure - comparison with numerical results

Normalized pressure perturbation,  $p/[\rho_0 U^2 l_0 h_0]$

$$\varepsilon = 0.1$$

$$n/l_0 = 2$$

$$l_0 a = 5$$



- Relative magnitude of pressure perturbation correctly predicted
- Some details of the flow different – e.g. absence of downstream maximum in blue curve

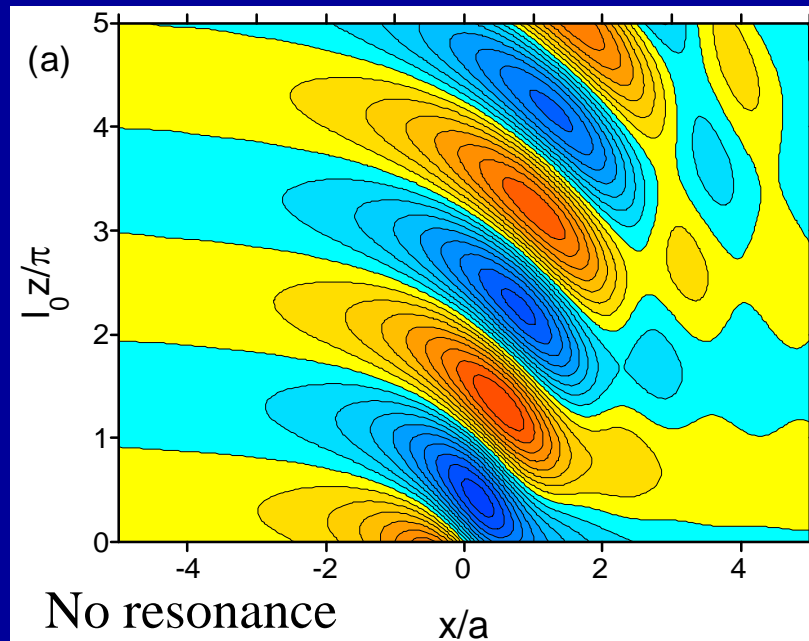
# Flow structure

Normalized vertical velocity perturbation field,  $w/[(h_0/a)U]$

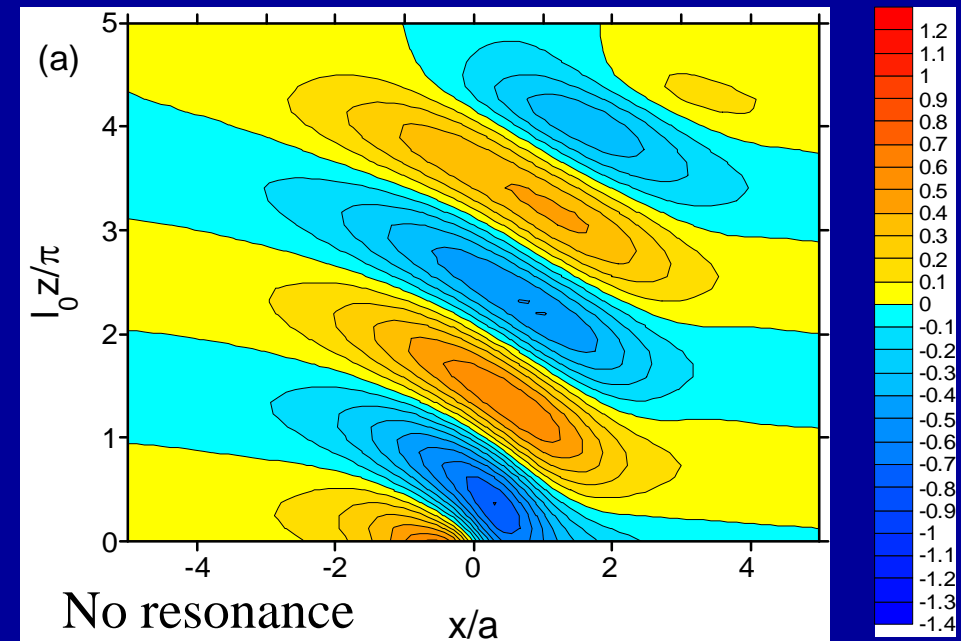
Non-resonant case:

$$\varepsilon = 0$$

$$l_0 a = 5$$



$$\lambda a / U = 2 \times 10^{-2}$$



Absorbing layer  
above  $l_0 z / \pi = 4$

# Flow structure

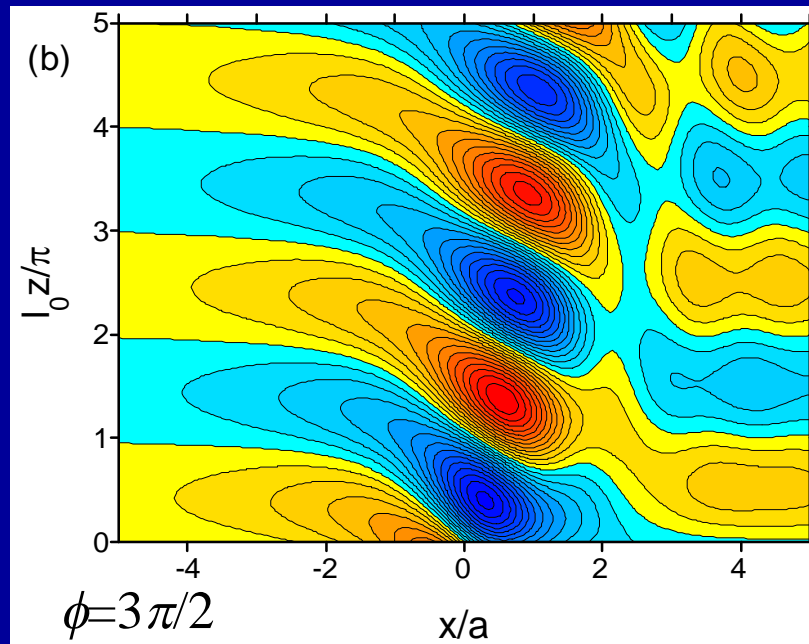
Normalized vertical velocity perturbation field,  $w/[(h_0/a)U]$

High-drag state:

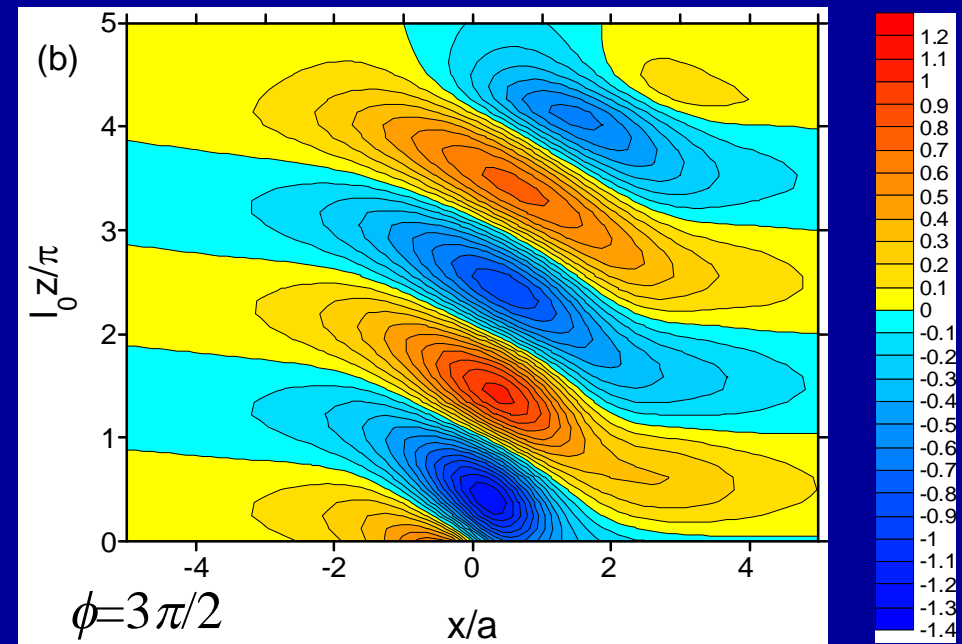
$$\varepsilon = 0.1$$

$$n/l_0 = 2$$

$$l_0 a = 5$$



$$\lambda a / U = 2 \times 10^{-2}$$



Absorbing layer  
above  $l_0 z / \pi = 4$

# Flow structure

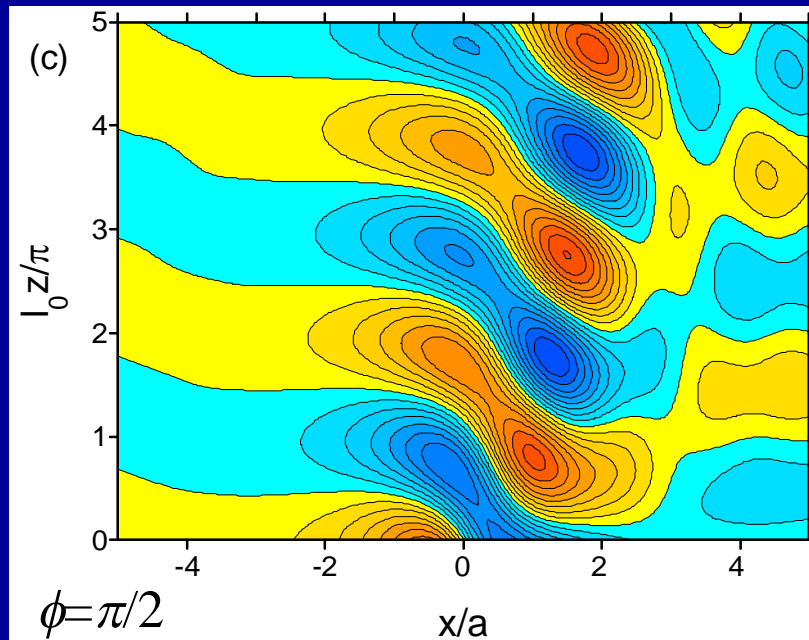
Normalized vertical velocity perturbation field,  $w/[(h_0/a)U]$

Low-drag state:

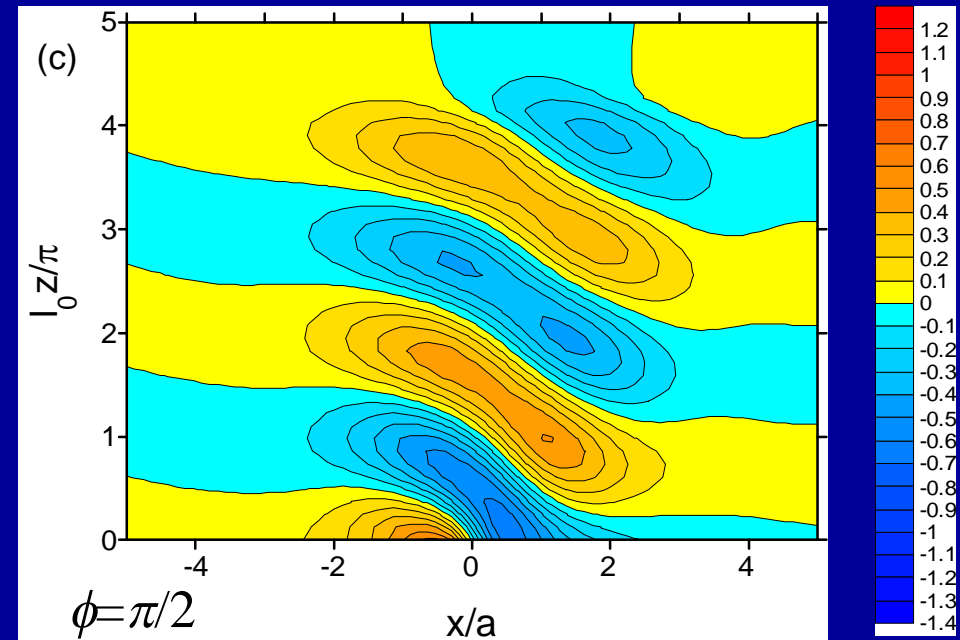
$$\varepsilon = 0.1$$

$$n/l_0 = 2$$

$$l_0 a = 5$$



$$\lambda a / U = 2 \times 10^{-2}$$



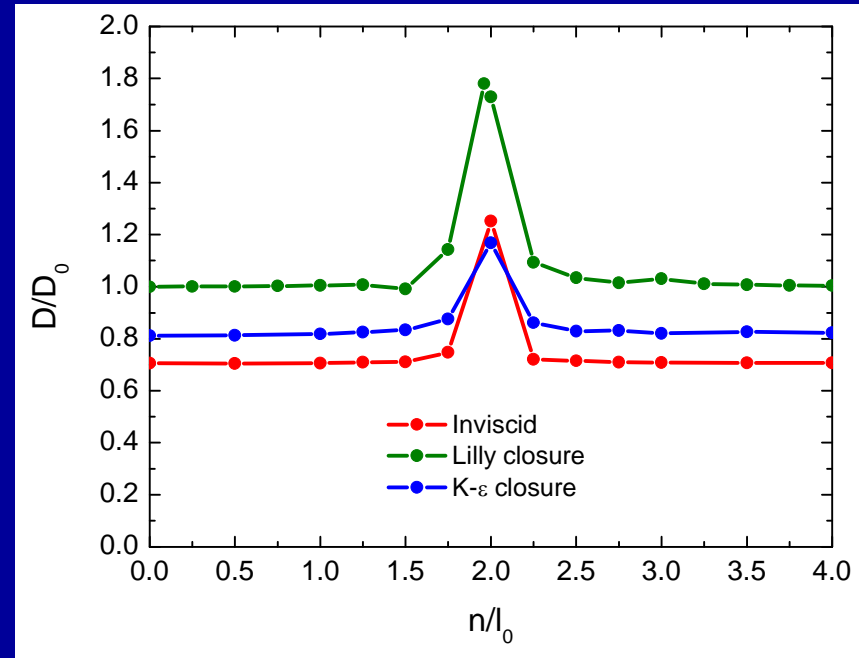
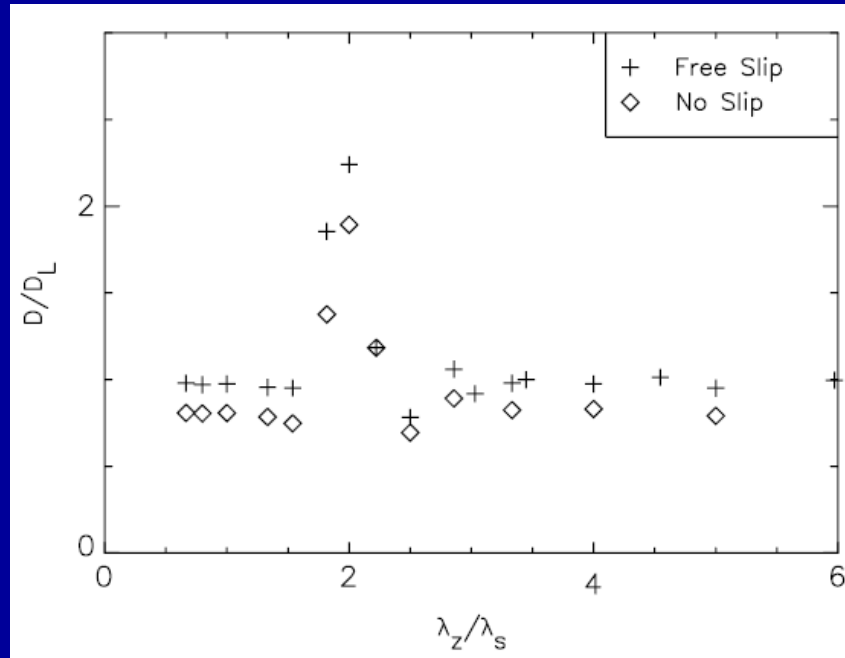
Absorbing layer  
above  $l_0 z / \pi = 4$

# Effect of turbulence closures

$$\varepsilon = 0.1$$

$$l_0 a = 5$$

$$\phi = 3\pi / 2$$



(from Wells and Vosper 2010)

- Smagorinsky-type or K- $\varepsilon$  turbulence closure
- M-O scaling in surface layer

- Large variation in drag behaviour depending on turbulence closure (and on numerical details in “inviscid” conditions)

# Summary

- Mountain wave drag may be significantly enhanced when Scorer parameter oscillates with height
- Gravity wave drag behaviour is reproduced qualitatively in linear framework including nonhydrostatic effects and friction
- Substantial fractional drag enhancement results from resonance when  $n/l_0 \approx 2$ , even if  $\varepsilon = 0.1$  - parametric resonance
- Friction has important impact on drag behaviour, generally moderating resonance
- However, when  $\phi = \pi/2$  or  $\phi = 3\pi/2$ , drag maxima or minima are totally suppressed in inviscid conditions
- Important for numerical models, because both turbulence closures and numerical dissipation introduce 'friction'
- Non-hydrostatic effects moderate resonance, because of wave dispersion

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